15-Day EXPRESS TERMS FOR PROPOSED BUILDING STANDARDS OF THE CALIFORNIA STATE LANDS COMMISSION

REGARDING AMENDMENTS TO CHAPTER 31F, MARINE OIL TERMINALS 2007 CALIFORNIA CODE OF REGULATIONS, TITLE 24, PART 2

(The State agency shall draft the regulations in plain, straightforward language, avoiding technical terms as much as possible and using a coherent and easily readable style. The agency shall draft the regulation in plain English. A notation shall follow the express terms of each regulation listing the specific statutes authorizing the adoption and listing specific statutes being implemented, interpreted, or made specific. (PART 1 – ADMINISTRATIVE CODE)

The following changes were made to the specific items in the Express Terms and therefore the Initial Statement of Reasons as a result of the comments received during the 60-day public review comment period. (Additions are identified with double underlines and deletions with double strikethroughs)

EXPRESS TERMS:

Authority: Section 8755 and 8757, Public Resources Code Reference(s): Section 8750, 8751, 8755 and 8757, Public Resources Code

FIGURE 31F-2-1

34. 3103F.5.7 Tsunamis. "...

For the San Francisco Bay, a recent study provides the maximum credible tsunami water levels and current speeds. These results are deterministic and are based on the most severe seismic sources that could reasonably impact MOTs in the San Francisco Bay [3.24]. Table 31F-3-8 provides values for the marine oil terminal locations within San Francisco Bay. Water levels could be positive or negative and current velocities may vary in direction. In order to determine the maximum run-up at a MOT, the largest values should be added to the maximum mean high tide. Further details are available in [3.24].

..."

Authority Cited: Sections 8755, and 8757, Public Resources Code Reference(s) Cited: Sections 8750, 8751, 8755, and 8757, Public Resources Code

42. 3103F.8 Load Combinations.

TABLE 31F-3-12
LRFD LOAD FACTORS FOR LOAD COMBINATIONS [3.43 26]

| Load Type | Vacant Condition | | Mooring & Breasting Condition | Berthing Condition | Earthquake Condition ³ | |
|-------------------------------------|----------------------------|------------|-------------------------------------|--------------------------|--|---------------------------|
| Dead Load (D) | 1. <u>2</u> 4 ¹ | 0.9 | 1.2 | 1.2 | 1.2+k ¹ 1±k ³ | <u>+ .9-k¹</u> |
| Live Load (L) | 1. <u>6</u> 7 ² | | 1. <u>6</u> ² 7 | <u>1.0</u> | <u>1.0</u> | |
| Buoyancy (B) | 1. <u>2</u> 3 | <u>0.9</u> | 1. <u>2</u> 3 | 1. <u>2</u> 3 | <u>1.2¹</u> | <u>0.9¹</u> |
| Wind on Structure (W) | 1. <u>6</u> 3 | <u>1.6</u> | 1. <u>6</u> 3 | 1. <u>6</u> 0 | | |
| Current on Structure (C) | 1. <u>2</u> 3 | <u>0.9</u> | 1. <u>2</u> 3 | 1. <u>2</u> 0 | <u>1.2</u> | <u>0.9</u> |
| Earth Pressure on the Structure (H) | 1.6 | <u>1.6</u> | 1.6 | 1.6 | 1. <u>6⁴ 0</u> | 1.6 ⁴ |
| Mooring/Breasting Load (M) | | | 1. <u>6</u> 3 | | | |
| Berthing Load (B _e) | | | | 1. <u>6</u> 7 | | |
| Earthquake Load (E) | | | | | 1.0 | <u>1.0</u> |

^{1.} k = 0.50 (PGA) The k factor (k=0.5(PGA)) and Buoyancy (B) shall be applied to the vertical dead load (D) only, and not to the inertial mass of the structure. Reduce load factor for dead load (D) to 0.9 to check components for minimum axial load and maximum moment.

Authority Cited: Sections 8755, and 8757, Public Resources Code

Reference(s) Cited: Sections 8750, 8751, 8755, and 8757, Public Resources Code

^{2.} The load factor for live load (L) may be reduced to 1.3 for the maximum outrigger float load from a truck crane.

^{3.} k = 0.50 (PGA) 3. For Level 1 and 2 earthquake conditions with strain levels defined in Division 7, the Current on Structure (C) may not be required.

^{4.} An Earth Pressure on the Structure factor (H) of 1.0 may be used for pile or bulkhead structure.

TABLE 31F-3-13
SERVICE or ASD LOAD FACTORS FOR LOAD COMBINATIONS[3.26]

| Load Type | Vacant Condition | Mooring & Breasting Condition | Berthing Condition | Earthquake Condition | |
|-------------------------------------|---------------------|-------------------------------------|----------------------------|---|---------------------------|
| Dead Load (D) | 1.0 | 1.0 | 1.0 | 1+0.7k ¹ 1±0.7k ¹ | <u>1-0.7k¹</u> |
| Live Load (L) | 1.0 | 1.0 | 0.75 | | |
| Buoyancy (B) | 1.0 | 1.0 | 1.0 | <u>1.0</u> | <u>0.6</u> |
| Wind on Structure (W) | 1.0 | 1.0 | 1.0 <u>0.75</u> | | 1.0 |
| Current on Structure (C) | 1.0 | 1.0 | 1.0 | | |
| Earth Pressure on the structure (H) | 1.0 | 1.0 | 1.0 | 1.0 | <u>1.0</u> |
| Mooring/Breasting Load (M) | | 1.0 | | | |
| Berthing Load (B _e) | | | 1.0 | | |
| Earthquake Load (E) | | | | 0.7 | <u>0.7</u> |
| % Allowable Stress | 100 | 100 | 100 | 133 | 100 ² |

^{1.} k = 0.5 (PGA)

Authority Cited: Sections 8755, and 8757, Public Resources Code Reference(s) Cited: Sections 8750, 8751, 8755, and 8757, Public Resources Code

66. 3107F.2.5.4 Plastic Rotation.

TABLE 31F-7-5 LIMITS OF STRAIN

| Component Strain | Level 1 | Level 2 | |
|---------------------------------|--|--|--|
| MCCS Pile/deck hinge | $\epsilon_c \le 0.005 \ \underline{4}$ | $\epsilon_c \! \leq 0.025$ | |
| MCCS In-ground hinge | $\epsilon_c \le 0.005 \ \underline{4}$ | $\epsilon_c \! \leq 0.008$ | |
| MRSTS <u>Pile/deck hinge</u> | $\epsilon_s \leq 0.01$ | ε _s ≤0.05 | |
| MRSTS In-ground hinge | <u>ε_s≤ 0.01</u> | <u>ε_s≤ 0.01</u> <u>0.025</u> | |
| MPSTS In-ground hinge | $\epsilon_p \le 0.005$ (incremental) | $\epsilon_{p} \le \frac{0.0 - 4 - 15}{\text{(total strain)}} \frac{0.025}{\text{(total strain)}}$ | |

 $\begin{array}{ll} \text{MCCS} &=& \text{Maximum Concrete Compression Strain, } \epsilon_c \\ \text{MRSTS} &=& \text{Maximum Reinforcing Steel Tension Strain, } \epsilon_s \\ \text{MPSTS} &=& \text{Maximum Prestressing Steel Tension Strain, } \epsilon_p \end{array}$

^{2.} Increase in allowable stress shall not be used with these load combinations unless it can be demonstrated that such increase is justified by structural behavior caused by rate or duration of load. See ASCE 7 [3.11]

Authority Cited: Sections 8755, and 8757, Public Resources Code Reference(s) Cited: Sections 8750, 8751, 8755, and 8757, Public Resources Code

78. 3107F.4 Retaining Structures.

Retaining structures constructed of steel or concrete shall conform to AISC [7.8] or ACI 318 [7.5] respectively. For the determination of static and seismic loads on the sheet pile and sheet pile behavior, the following references are acceptable: NCEL [7.13], Strom and Ebeling [7.14], and PIANC TC-7(Technical Commentary-7) [7.15]. The applied loads and analysis methodology shall be determined by a California Registered Geotechnical Engineer, and are may be subject to peer review prior to submission to the Division.

Authority Cited: Sections 8755, and 8757, Public Resources Code Reference(s) Cited: Sections 8750, 8751, 8755, and 8757, Public Resources Code

85.

3108F.6.2 Fire Hydrants. Hydrants shall be located not greater than 150 300 ft. apart, along the wharf and not more than 300 ft. apart on the approach trestle [Section 4.2.3 of API 2001 [8.1 4]. (N) Additional hose connections shall be provided at the base of fixed monitors and upstream of the water and foam isolation valves. Connections shall be accessible to fire trucks or mutual aid equipment as identified in the Fire Plan (N).

Hydrants and hoses shall be capable of applying two independent water streams covering the cargo manifold, transfer system, sumps and vessel manifold (N/E).

Authority Cited: Sections 8755, and 8757, Public Resources Code Reference(s) Cited: Sections 8750, 8751, 8755, and 8757, Public Resources Code